THESIS

A brief note on ellipse kinematics

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ABSTRACT

The movement of a material point along curves of the second order is represented by the kinematic equation (1.10). The kinematics of second order curves is studied on an ellipse. Formulas for the dependence of

INTRODUCTION

Lf simple equations of speed and acceleration are sufficient to describe rectilinear motion: V=S/t, $a=S/t^2$, then differential equations of motion are needed to solve problems on the curvilinear motion of material points and their systems. "The way we derive these equations doesn't matter": $(1, \$11, \pi.$ 3)

Formulas for the dependence of acceleration and radius, speed and radius

ddy dy C(x,y)X Figure 1: For the dependence of acceleration and radius, speed and radius.

There is a system of equations for a parametric pendulum (1) The parameter is time (t).

$$\begin{cases} x = r(\varphi(t)) \cdot \cos(\varphi(t)) \\ \mathbf{y} = r(\varphi(t)) \cdot \sin(\varphi(t)) \end{cases}$$
(1.1)

Let us substitute into system (1) the radius of the ellipse with respect to the focus:

acceleration and radius, speed and radius are derived. The direction of the velocity and acceleration vectors is determined. The conditions for the conservation of Kepler's laws when a material point moves along an ellipse are shown.

Keywords: Kepler's laws; Ellipse; Speed; Acceleration; Radius

$$r(\varphi(t)) = \frac{b^2}{a(1 - e * cos(\varphi(t)))}$$
(1.2)

$$\begin{cases} x = \frac{b^2}{a(1 - e * cos(\varphi(t)))} \cdot cos(\varphi(t)) \\ y = \frac{b^2}{a(1 - e * cos(\varphi(t)))} \cdot sin(\varphi(t)) \end{cases}$$
(1.3)

Let's differentiate twice. We get the coordinates of speed and acceleration:

$$\dot{x} = \frac{d}{dt} \left(r\left(\varphi(t)\right) \cos(\varphi(t)) \right) = -\frac{b^2 \cdot \dot{\varphi} \cdot \sin(\varphi(t))}{a(e^* \cos(\varphi(t)) - 1)^2} = \frac{r^2 \cdot \dot{\varphi} \cdot \sin(\varphi(t))}{e^* \cos(\varphi(t)) - 1}$$
(1.4)

$$\dot{y} = \frac{d}{dt} \left(\frac{p}{1 - e^* \cos(\varphi(t))} \sin(\varphi(t)) \right) = \frac{b^2 \cdot \dot{\varphi} \cdot (-e^+ \cos(\varphi(t)))}{a \left(e^* \cos(\varphi(t)) - 1\right)^2} = \frac{r^2 \cdot \varphi \cdot (-e^+ \cos(\varphi(t)))}{1 - e^* \cos(\varphi(t))}$$
(1.5)

$$\ddot{x} = \frac{b^2 \left(\left(-e * \cos(\varphi(t)) * \sin(\varphi(t)) \right) \ddot{\varphi} + \dot{\varphi}^2 \left(e^* \cos(\varphi(t))^2 - 2e + \cos(\varphi(t)) \right) \right)}{a \left(e^* \cos(\varphi(t)) - 1 \right)^3}$$
(1.6)

$$\ddot{y} = \frac{-b^2 \left(\left(-\cos(\varphi(t))(e * \cos(\varphi(t)) - 1) + e\right) \ddot{\varphi} + 2\dot{\varphi}^2 \left(e^2 - \frac{e * \cos(\varphi(t)) + 1}{2} \right) \sin(\varphi(t)) \right)}{a(e * \cos(\varphi(t)) - 1)^2}$$
(1.7)

Acceleration $\dot{v} = \sqrt{\ddot{x}^2 + \ddot{y}^2} =$

$$b^{2}\begin{pmatrix} \frac{\sqrt{(e^{2}-2e^{*}cos(\varphi(t))+1)(e^{*}cos(\varphi(t))-1)^{2}*\ddot{\varphi}^{2}}{a(e^{*}cos(\varphi(t))-1)^{2}}+\\ \frac{\sqrt{4(e^{2}-\frac{2ie^{*}cos(\varphi(t))+1}{2})\dot{\varphi}^{2}(e^{*}cos(\varphi(t))sin(\varphi(t))-1)\ddot{\varphi}}{a(e^{*}cos(\varphi(t))-1)^{3}}-\\ \frac{\sqrt{4\dot{\varphi}^{4}(-cos(\varphi(t))^{2}e^{2}+(e^{4}-\frac{e^{2}}{4})cos(\varphi(t))^{2}+(e^{2}+\frac{\theta}{2})cos(\varphi(t))-e^{4}-\frac{1}{4})}{a(e^{*}cos(\varphi(t))-1)^{3}}\end{pmatrix}$$
(1.9)

We form a system of equations from (1.6), (1.7) and solve for ϕ . We obtain the kinematic equation of motion of a point relative to the focus along second order curves:

$$\ddot{\varphi} = \frac{2 \cdot e \cdot \sin(\varphi) \cdot \dot{\varphi}^2}{1 - e \cdot \cos(\varphi)} \tag{1.10}$$

At different values of eccentricity, the shape of the curve will change [1].

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Point C moves in an ellipse relative to the focus (Figure 1).

Viktor S

We substitute (1.10) into (1.9), and simplify:

$$\dot{v} = \frac{b^2 \dot{\varphi}^2}{a(1 - e * \cos(\varphi))^2} = \frac{r * \dot{\varphi}^2}{1 - e * \cos(\varphi)}$$
(1.11)

The sector speed is constant:

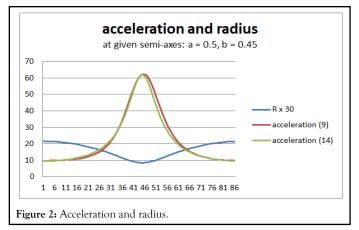
$$k = r_p^2 * \dot{\phi}_p = r_i^2 * \dot{\phi}_i = r_a^2 * \dot{\phi}_a = const, \qquad (1.12)$$

$$\dot{\phi} = \frac{k}{r^2} \qquad (1.13)$$

where r_p is the perifocal distance, r_a is the apofocal distance We substitute (1.13) into (1.11):

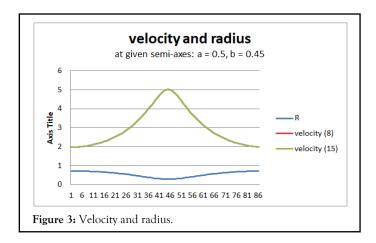
$$\dot{v} = \frac{k^2}{r^3(1-e*\cos(\varphi))}$$
 (1.14)

The acceleration v $\dot{}$ is recalculated using formula (14). Results (9) and (14) are compared (Figures 2 and 3).



We substitute (1.13) into (1.8):

$$v = \frac{r * k * \sqrt{1 + e^2 - 2e * \cos\varphi(t)}}{r^2 (1 - e^* \cos\varphi(t))} = \frac{k * \sqrt{1 + e^2 - 2e * \cos\varphi(t)}}{r * (1 - e^* \cos\varphi(t))}$$
(1.15)



Formulas (1.14, 1.15) do not give any advantage for calculating the modulus of speed and acceleration. First, to calculate the sector constant k, you need to calculate the angular velocity once. Secondly, in order for the motion of a point to comply with Kepler's laws, the angle must change according to elliptic equations. The value of these formulas is in the logical definition of the dependence of speed and acceleration on the radius [2].

Velocity and acceleration vectors

Let's consider two variants of point movement, Figure 4: a) Movement relative to the center; b) Movement relative to the focus.

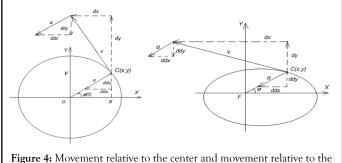
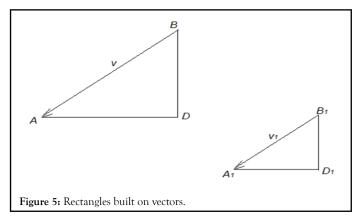


Figure 4: Movement relative to the center and movement relative to the focus.

Note: v-speed, a-acceleration, dx, dy, ddx, ddy-first and second derivatives along the coordinate axes.

Note the property of collinear vectors on the plane rectangles built on vectors, Figure 5, should be similar:





Movement relative to focus

Let's compare the ratio of the coordinates of the radius and acceleration:

$$\frac{x}{y} = \frac{\cos\varphi}{\sin\varphi} \tag{2.2}$$

$$\frac{\ddot{x}}{\ddot{y}} = \frac{(-2e^2\cos^2\varphi + 3e^2 - 1)\cos(\varphi)}{\sin(\varphi)(e^2 - 1)(2e^2\cos^2\varphi + 1)}$$
(2.3)

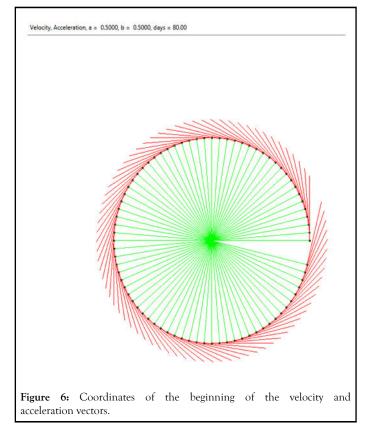
If
$$e = 0$$
 we get a circle and $\frac{\ddot{x}}{\ddot{y}} = \frac{x}{y}$, (2.4)

A special case of an ellipse.

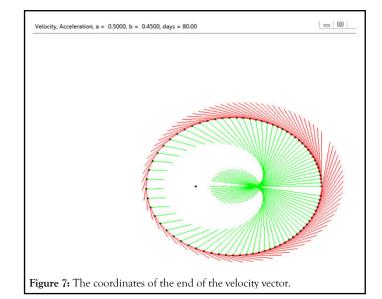
In Figures 5-7 they are marked with red lines for speed, green for acceleration [3].

$$\frac{d^2}{dt^2}\varphi(t) = 0,$$
 рисунок 6 (2.5)

Coordinates of the beginning of the velocity and acceleration vectors, points of the initial ellipse (x,y). The coordinates of the end of the velocity vector (dx+x, dy+y). Acceleration vector end coordinates (ddx+x, ddy+y) [4].



If
$$e \neq 0$$
, then $\frac{\ddot{x}}{\ddot{y}} \neq \frac{x}{y}$, (2.6)



Movement relative to the center

$$r(\varphi(t)) = \frac{b}{\sqrt{1 - e^2 \cos^2 \varphi(t)}}$$
(2.7)

To derive the kinematic equation of motion of a point relative to the center, we will replace the radius formula (2) with (13) in the system of equations (1.1) [5].

Let's differentiate twice. We get the coordinates of speed and acceleration:

$$\dot{x} = \frac{d}{dt} \left(\frac{b * \cos(\varphi(t))}{\sqrt{1 - e^2 * \cos(\varphi(t))^2}} \right) = -\frac{b * \sin(\varphi)}{(1 - e^2 * \cos^2 \varphi)^{2/2}}$$
(2.8)

$$\dot{y} = \frac{d}{dt} \left(\frac{b * sin(\varphi(t))}{\sqrt{1 - e^2 * cos(\varphi(t))^2}} \right) = \frac{b(1 - e^2) cos(\varphi)}{(1 - e^2 * cos^2 \varphi)^{3/2}}$$
(2.9)

$$\ddot{x} = \frac{d^2}{dt^2} \left(\frac{b * cos(\varphi(t))}{\sqrt{1 - e^2 * cos(\varphi(t))^2}} \right) = -\frac{b * cos(\varphi) (2e^2 cos^2 \varphi - 3e^2 + 1)}{(1 - e^2 * cos^2 \varphi)^{5/2}}$$
(2.10)

$$\ddot{y} = \frac{d^2}{dt^2} \left(\frac{b * sin(\varphi(t))}{\sqrt{1 - e^2 * cos(\varphi(t))^2}} \right) = \frac{b * sin(\varphi)(e^2 - 1)(2e^2 \cos^2 \varphi + 1)}{(1 - e^2 * cos^2 \varphi)^{8/2}}$$
(2.11)

$$v = \sqrt{\dot{x}^2 + \dot{y}^2} = \sqrt{\frac{b^2 \dot{\varphi}^2 \left(1 - 2e^2 \cos(\varphi(t))^2 + e^4 \cos(\varphi(t))^2\right)}{\left(1 - e^2 \cos(\varphi(t))^2\right)^3}}$$
(2.12)

We solve for ϕ . We obtain the kinematic equation of motion of a point relative to the center along second order curves:

$$\ddot{\varphi} = \frac{2 * e^2 * \cos(\varphi) * \sin(\varphi) * \dot{\varphi}^2}{1 - e^2 * \cos(\varphi)^2}$$
(2.13)

Let's compare the ratio of the coordinates of the radius and acceleration:

Viktor S

$$\frac{x}{y} = \frac{\cos\varphi}{\sin\varphi} \tag{2.14}$$

$$\frac{\ddot{x}}{\ddot{y}} = \frac{(-2e^2\cos^2\varphi + 3e^2 - 1)\cos(\varphi)}{\sin(\varphi)(e^2 - 1)(2e^2\cos^2\varphi + 1)}$$
(2.15)

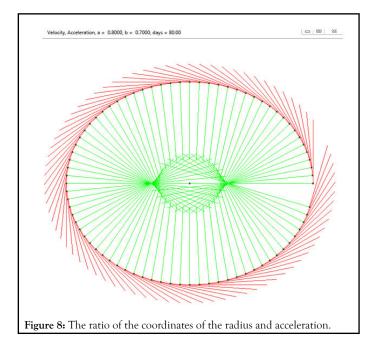
If
$$e = 0$$
 we get a circle and $\frac{\ddot{x}}{\ddot{y}} = \frac{x}{y}$, (2.16)

A special case of an ellipse, Figure 8.

Eccentricity e=0. Substitute in equation (2.15)

$$\frac{d^2}{dt^2}\varphi(t) = 0,$$

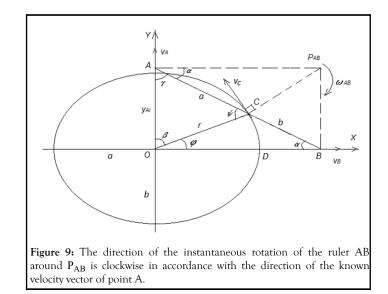
If $e \neq 0$, then $\frac{\ddot{x}}{\ddot{y}} \neq \frac{x}{y}$, (2.17)



Trammel of archimedes

Any point on the ellipsograph ruler moves along an elliptical path around the center.

In order not to refer the reader to the sources, we present the derivation of the formulas necessary for calculating velocities, accelerations, and rotation angles (Figure 9) [6].



Ruler AB moves from horizontal to vertical position, Figure 9. Point C describes $\frac{1}{4}$ of the ellipse. The direction of the instantaneous rotation of the ruler AB around P_{AB} is clockwise in accordance with the direction of the known velocity vector of point A.

Speeds of points B and C:

$$\omega_{AB} = \frac{v_A}{AP_{AB}} \tag{3.1}$$

$$v_B = \omega_{AB} * BP_{AB} = v_A \frac{BP_{AB}}{AP_{AB}}$$
(3.2)

Vector v_C is directed perpendicular to CP.

$$v_{C} = \omega_{AB} * CP_{AB} = v_{A} \frac{CP_{AB}}{AP_{AB}}$$
(3.3)

The directions of the velocities of the points and are determined by the instantaneous rotation of the ruler AB around the instantaneous center of velocities P_{AB} .

Determination of accelerations of points B and C

Let's use the theorem acceleration of points of a flat figure. Point A will be a pole, since the acceleration of point A is known.

The vector equation for the acceleration of point B has the form:

$$\overrightarrow{a_B} = \overrightarrow{a_A} + \overrightarrow{a_{BA}^r} + \overrightarrow{a_{BA}^c}$$
(3.4)

Where $\overline{a_A}$ is the acceleration of the pole A (given);

 $\overline{a_{k,a}^r}$ and $\overline{a_{k,a}^r}$ are the rotational and centripetal accelerations of the point B in the rotation of the ruler around the pole A. In this case:

$$a_{BA}^c = \omega_{AB}^2 * BA \tag{3.5}$$

The vector $\overline{\alpha_B}$ is located perpendicular to the ruler AB, its direction is unknown, since the direction of the angular acceleration ϵ_{AB} is unknown.

In equation (3.4) there are two unknowns: Accelerations \bar{v}_{i} and $\bar{a}_{i,a}^{r}$, which can be determined from the equations of vector equality projections onto the directions of axes AX and AY:

The direction of the vectors and is chosen arbitrarily. The solution of system (3.6) allows one to find the numerical value and with a plus or minus sign. A positive value indicates the correctness of the chosen direction of the vectors and a negative value indicates the need to change their direction (Figure 10).

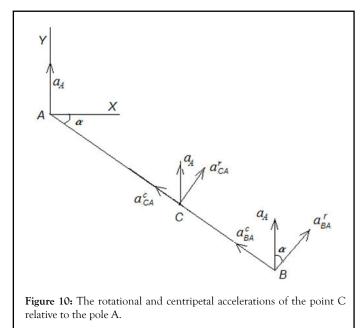
$$a_{A} = \sqrt{(a_{Ax})^{2} + (a_{Ay})^{2}}, \ a_{AB}^{r} = \sqrt{(a_{ABx}^{r})^{2} + (a_{ABy}^{r})^{2}}$$
(3.7)

Ruler angular acceleration:

$$\boldsymbol{\varepsilon}_{AB} = \frac{a_{BA}^r}{BA} \tag{3.8}$$

The acceleration of point C is determined by the equation:

$$\overrightarrow{a_{\mathcal{C}}} = \overrightarrow{a_{\mathcal{A}}} + \overrightarrow{a_{\mathcal{C}\mathcal{A}}^{r}} + \overrightarrow{a_{\mathcal{C}\mathcal{A}}^{c}}$$
(3.9)



Where $\overline{a_{cA}^r}$ and $\overline{a_{cA}^c}$ are, respectively, the rotational and centripetal accelerations of the point C relative to the pole A:

$$a_{CA}^{c} = \omega_{AB}^{2} * AC \qquad (3.10)$$
$$a_{CB}^{r} = \varepsilon_{AB} * AC \qquad (3.11)$$

Vector $\overline{a_{e_A}^c}$ is located on CA and is directed from point C to pole A. Vector $\overline{a_{e_A}^c}$ is perpendicular to CA and directed in the same direction as $\overline{a_{b_A}^c}$.

Equation (3.10) can be represented in projections on the axes Ax and Ay:

$$\begin{cases} \boldsymbol{a}_{Cx} = \boldsymbol{a}_{Ax} + \boldsymbol{a}_{CAx}^{c} + \boldsymbol{a}_{CAx}^{r} \\ \boldsymbol{a}_{Cy} = \boldsymbol{a}_{Ay} + \boldsymbol{a}_{CAy}^{c} + \boldsymbol{a}_{CAy}^{r} \end{cases}$$
(3.12)

The acceleration projections of point C are determined from (3.10). The direction of the vector $\overline{a_c}$ is determined by the signs of the projections a_{Cx} and a_{Cy} .

Vector modulus:

$$a_{C} = \sqrt{(a_{Cx})^{2} + (a_{Cy})^{2}}$$
(3.13)

Let's take a look at the different travel options

T is the period specified by arbitrary units of time. AB=a+b, A(0,y_A) B(x_B, 0). Initial coordinates of points: A(0,0), B(a+b,0), C(a,0). Initial speed $v_{A0}{=}0.$

Uniform movement

Given: point C divides AB into segments a and b, A(0,y_A), B(x_B,0), initial A(0,0), B(AB,0). A moves uniformly from $O \rightarrow Y$. Accelerations $a_A=0$, $a_B=0$, speed

$$v_A = \frac{AB*4}{T} \tag{3.14}$$

Find:
$$y_{A_i}$$
, x_{C_i} , y_{C_i} , v_{C_i} , a_{C_i} , ϕ_i

Solution

Coordinates $A(0, y_{A_i})$:

$$y_{A_i} = v_A * i \tag{3.15}$$

Further, according to equations (3.4)-(3.14)

$$\sin \alpha = \frac{y_{Ai}}{AB}, \, \alpha = \operatorname{asin} \frac{y_{Ai}}{AB} \tag{3.16}$$

$$x_{B_i} = \cos \alpha * AB, y_{B_i} = 0 \tag{3.17}$$

$$\boldsymbol{\omega}_{AB} = \frac{\boldsymbol{v}_A}{\boldsymbol{AP}_{AB}} = \frac{\boldsymbol{v}_A}{\boldsymbol{x}_{B_i}} \tag{3.18}$$

$$\boldsymbol{v}_B = \boldsymbol{\omega}_{AB} * B\boldsymbol{P}_{AB} = \boldsymbol{\omega}_{AB} * \boldsymbol{y}_{A_i} \tag{3.19}$$

From equation (5) $a_{BA}^c = \omega_{AB}^2 * BA$

$$\begin{cases} \boldsymbol{a}_{Bx} = \boldsymbol{a}_{BA}^{c} * \cos \alpha + \boldsymbol{a}_{BA}^{r} * \sin \alpha \\ \boldsymbol{0} = \boldsymbol{a}_{Ay} + \boldsymbol{a}_{BA}^{c} * \sin \alpha + \boldsymbol{a}_{BA}^{r} * \cos \alpha \end{cases}$$
(3.20)

Solving the resulting equations, we find a_B ,

Viktor S

$$a_{BA}^{r} = \frac{-a_{Ay} - a_{BA}^{r} \sin \alpha}{\cos \alpha} = \frac{-a_{BA}^{r} \sin \alpha}{\cos \alpha}$$
(3.21)
$$\mathbf{c} = -\frac{a_{BA}^{r}}{\cos \alpha}$$
(3.22)

$$\varepsilon_{AB} = \frac{a_{BA}}{AB} \tag{3.22}$$

Coordinates $P_{AB}(x_{B_i}, y_{A_i})$

Coordinates
$$C(x_{C_i}, y_{C_i})$$

 $\frac{a}{AB} = \frac{x_{C_i}}{x_{B_i}}, \frac{b}{AB} = \frac{y_{C_i}}{y_{A_i}}$
(3.23)

$$x_{C_{i}} = \frac{a}{AB} * x_{B_{i}}, y_{C_{i}} = \frac{b}{AB} * y_{A_{i}}$$
(3.24)

$$CP_{AB} = \sqrt{x_{B_i}^2 + a^2 - 2(a * x_{B_i})\cos\alpha}$$
(3.25)

$$v_{C} = \omega_{AB} * CP_{AB} = \omega_{AB} * \sqrt{x_{B_{i}}^{2} + a^{2} - 2 * (a * x_{B_{i}}) * \cos \alpha}$$
(3.26)

$$\varphi = \operatorname{atan} \frac{y_{C_i}}{x_{C_i}} \tag{3.27}$$

$$\boldsymbol{a}_{CA}^{c} = \boldsymbol{\omega}_{AB}^{2} * AC = \boldsymbol{\omega}_{AB}^{2} * a \tag{3.28}$$

$$\boldsymbol{a}_{CA}^{r} = \boldsymbol{\varepsilon}_{AB} * AC = \boldsymbol{\varepsilon}_{AB} * a \tag{3.29}$$

$$\begin{cases} a_{Cx} = a_{Ax} + a_{CAx}^{r} + a_{CAx}^{c} \\ a_{Cy} = a_{Ay} + a_{CAy}^{r} + a_{CAy}^{c} \end{cases}$$
(3.30)

$$\begin{cases} \boldsymbol{a}_{Cx} = 0 + \boldsymbol{a}_{CA}^{r} * \sin \alpha + \boldsymbol{a}_{CA}^{c} * \cos \alpha \\ \boldsymbol{a}_{Cy} = 0 + \boldsymbol{a}_{CA}^{r} * \cos \alpha + \boldsymbol{a}_{CA}^{c} * \sin \alpha \end{cases}$$
(3.31)

$$a_{C} = \sqrt{a_{Cx}^{2} + a_{Cy}^{2}}$$
(3.32)

Uniformly accelerated motion

Given: point C divides AB into segments a and b, A moves uniformly accelerated from O \rightarrow Y, A(0,y_A) B(x_B,0), initial A(0,0), B(AB,0),

 $a_{A_i}=const, v_{A_0}=0.$

Find: y_{A_i} , (x_{C_i}, y_{C_i}) , $v_{C_i}, a_{C_i}, \varphi_i$

Solution

$$v_{A_i} = \frac{a_A \cdot i^2}{2}; \quad i = 1 \dots n = \frac{T}{4}$$
 (3.33)

$$AB = v_{An} = \frac{a_A * n^2}{2} \tag{3.34}$$

$$a_{A_i} = a_A = \frac{2AB}{n^2}$$
(3.35)

Coordinates $A(0, y_{A_i})$

$$y_{A_i} = \frac{a_A * i^2}{2} \tag{3.36}$$

Further, according to equations (3.4)-(3.14)

Coordinates $B(x_{B_i}, 0)$:

$$x_{B_i} = \sqrt{AB^2 - y_{A_i}^2} \tag{3.37}$$

Coordinates $C(x_{C_i}, y_{C_i})$:

$$\frac{a}{AB} = \frac{x_{C_i}}{x_{B_i}}, \frac{b}{AB} = \frac{y_{C_i}}{y_{A_i}}$$
(3.38)

$$x_{C_i} = \frac{a}{AB} * x_{B_i}, y_{C_i} = \frac{b}{AB} * y_{A_i}$$
(3.39)

$$\boldsymbol{\omega}_{AB} = \frac{\boldsymbol{v}_{Ai}}{A\boldsymbol{P}_{AB}} = \frac{\boldsymbol{v}_{Ai}}{\boldsymbol{x}_{Bi}} \tag{3.40}$$

$$\boldsymbol{a}_{BA}^{c} = \boldsymbol{\omega}_{AB}^{2} * AB \tag{3.41}$$

$$\boldsymbol{a}_{BA}^r = \boldsymbol{\varepsilon}_{AB} * BA \tag{3.42}$$

The vector $\overline{a_{BA}^{\epsilon}}$ is located perpendicular to the ruler AB, its direction is unknown, since the direction of the angular acceleration ε_{AB} is unknown. We project the vector equation (3.4) on the coordinate axis:

$$\begin{cases} \boldsymbol{a}_{Bx} = \boldsymbol{a}_{BA}^{c} * \cos \alpha + \boldsymbol{a}_{BA}^{r} * \sin \alpha \\ \boldsymbol{0} = \boldsymbol{a}_{Ay} + \boldsymbol{a}_{BA}^{c} * \sin \alpha + \boldsymbol{a}_{BA}^{r} * \cos \alpha \end{cases}$$
(3.43)

Solving the resulting equations, we find a_B :

$$a_{BA}^r = \frac{-a_{Ay} - a_{BA}^c \sin \alpha}{\cos \alpha} \tag{3.44}$$

$$\boldsymbol{\varepsilon}_{AB} = \frac{a_{BA}^r}{AB} \tag{3.45}$$

Equation (10) can be represented in projections on the axes Ax and Ay:

$$\begin{cases} \boldsymbol{a}_{Cx} = \boldsymbol{a}_{Ax} + \boldsymbol{a}_{CAx}^r + \boldsymbol{a}_{CAx}^c \\ \boldsymbol{a}_{Cy} = \boldsymbol{a}_{Ay} + \boldsymbol{a}_{CAy}^r + \boldsymbol{a}_{CAy}^c \end{cases}$$
(3.46)

$$\begin{cases} \boldsymbol{a}_{Cx} = 0 + \boldsymbol{a}_{CA}^r * \sin \alpha + \boldsymbol{a}_{CA}^c * \cos \alpha \\ \boldsymbol{a}_{Cy} = \boldsymbol{a}_A + \boldsymbol{a}_{CA}^r * \cos \alpha + \boldsymbol{a}_{CA}^c * \sin \alpha \end{cases}$$
(3.47)

$$a_{C} = \sqrt{a_{Cx}^{2} + a_{Cy}^{2}} \tag{3.48}$$

Elliptical (Keplerian)

The movement of the points of the ruler along the ellipse relative to the center,

$$\ddot{\varphi} = \frac{2*e^2*\cos(\varphi)*\sin(\varphi)*\dot{\varphi}^2}{1-e^2*\cos(\varphi)^2}$$

Given: point C divides AB into segments a and b, A moves elliptically according to the formula (2.13), from $O \rightarrow Y$, A(0,y_A), B(x_B,0), initial A(0,0), B(AB,0),

$$v_{A_0} = 0.$$

Find: $y_{A_i}, x_{C_i}, y_{C_i}, v_{C_i}, a_{C_i}$.

Solution

Equation (2.13) calculates φ_i , x_{C_i} , y_{C_i}

$$\alpha = \arcsin \frac{y_c}{b} \tag{3.49}$$

$$\beta = \frac{\pi}{2} - \varphi_i \tag{3.50}$$

$$\gamma = \arcsin\left(\frac{r_i * \sin\beta}{a}\right) \tag{3.51}$$

$$\psi = \pi - \gamma - \beta \tag{3.52}$$

$$y_{A_i} = \frac{y_{C_i} + a \cdot \sin \alpha}{b} \tag{3.53}$$

$$v_{A_i} = y_{A_i} - y_{A_{i-1}} \tag{3.54}$$

$$a_{A_i} = v_{A_i} - v_{A_{i-1}} \tag{3.55}$$

Further, according to equations (3.4)-(3.14)

Coordinates $B(x_{B_i}, 0)$:

$$x_{B_i} = \sqrt{AB^2 - y_{A_i}^2} \tag{3.56}$$

Find the coordinates $C(x_{C_i}, y_{C_i})$ again:

$$\frac{a}{AB} = \frac{x_{C_i}}{x_{B_i}}, \frac{b}{AB} = \frac{y_{C_i}}{y_{A_i}}$$
(3.57)

$$x_{C_i} = \frac{a}{AB} * x_{B_i}, y_{C_i} = \frac{b}{AB} * y_{A_i}$$
(3.58)

$$\boldsymbol{\omega}_{AB} = \frac{\boldsymbol{v}_{Ai}}{A\boldsymbol{P}_{AB}} = \frac{\boldsymbol{v}_{Ai}}{\boldsymbol{x}_{Bi}} \tag{3.59}$$

$$\boldsymbol{a}_{BA}^{c} = \boldsymbol{\omega}_{AB}^{2} * AB \tag{3.60}$$

$$\boldsymbol{a}_{BA}^r = \boldsymbol{\varepsilon}_{AB} * BA \tag{3.61}$$

The vector $\overline{\alpha_{BA}}$ is located perpendicular to the ruler AB, its direction is unknown, since the direction of the angular acceleration ε_{AB} is unknown.

We project the vector equation (3.4) on the coordinate axis:

$$\begin{cases} \boldsymbol{a}_{Bx} = \boldsymbol{a}_{BA}^{c} * \cos \alpha + \boldsymbol{a}_{BA}^{r} * \sin \alpha \\ \boldsymbol{0} = \boldsymbol{a}_{Ay} + \boldsymbol{a}_{BA}^{c} * \sin \alpha + \boldsymbol{a}_{BA}^{r} * \cos \alpha \end{cases}$$
(3.62)

Solving the resulting equations, we find a_B ,

$$\boldsymbol{a}_{BA}^{r} = \frac{-\boldsymbol{a}_{AY} - \boldsymbol{a}_{BA}^{r} + \sin\alpha}{\cos\alpha} \tag{3.63}$$

$$\varepsilon_{AB} = \frac{a_{BA}^r}{AB} \tag{3.64}$$

The acceleration of point C is determined by equation (3.10): $\overrightarrow{a_{C}} = \overrightarrow{a_{A}} + \overrightarrow{a_{CA}^{r}} + \overrightarrow{a_{CA}^{c}}$

$$\begin{aligned} &a_{CA}^{c} = \omega_{AB}^{2} * AC = \omega_{AB}^{2} * a \end{aligned} \tag{3.65} \\ &a_{CA}^{r} = \varepsilon_{AB} * AC = \varepsilon_{AB} * a \end{aligned} \tag{3.66}$$

Equation (3.10) can be represented in projections on the axes Ax and Ay:

$$\begin{cases} a_{Cx} = a_{Ax} + a_{CAx}^{c} + a_{CAx}^{c} \\ a_{Cy} = a_{Ay} + a_{CAy}^{r} + a_{CAy}^{c} \end{cases}$$
(3.67)
$$\begin{cases} a_{Cx} = 0 + a_{CA}^{r} * \sin \alpha + a_{CA}^{c} * \cos \alpha \\ a_{Cy} = a_{A} + a_{CA}^{r} * \cos \alpha + a_{CA}^{c} * \sin \alpha \end{cases}$$
(3.68)
$$a_{C} = \sqrt{a_{Cx}^{2} + a_{Cy}^{2}}$$
(3.69)

The obtained motion parameters allow checking the fulfillment of Kepler's laws.

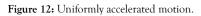
Kepler's second law

Equality of the areas of sectors is carried out only with elliptical motion (Figure 11-13).

Enter char = if char = "y" then the source data is specified: y = 0.550, $b = 0.450$, $T = 250$
a = 0.500; b = 0.450; T = 360 Second law of Kepler
Point bypasses 1/4 ellipse counterclockwise in 89 time units Input 0 - uniform motion OR Input 1-uniformmly accelerated motion OR, Input 2- elliptical motion>:
UNIFORM MOTION Set the start of the first sector (1,, 89): 3 Set the end of the first sector (3< end (89):17 Set the start of the second sector (1,, 89): 55 first sector: angle(start)= 0.03; angle(end)= 0.17
second secto: angle(start)= 0.61 ; angle(end) = 0.82 intervals of time t1= 14; t2= 14
Area of the first sector: 0.1767757E-01 IERR: 0
Area of the second sector: 0.2445188E-01 IERR: 0

Figure 11: Uniform movement.

Enter c	
y	"y" then the source data is specified: 00; b = 0.450; T = 360
Point by Input Input	law of Kepler passes 1/4 ellipse counterclockwise in 89 time units 8 - uniform motion OR 1-uniformly accelerated motion OR, 2- elliptical motion):
Set the Set the first second interv	LLY ACCELERATEM MOTION start of the first sector $(1, \ldots, 89)$: 3 end of the first sector $(3 < end < 89)$:17 start of the second sector $(1, \ldots, 89)$: 55 sector: angle $(start) = 0.00$; angle $(end) = 0.03$ (sector: angle $(start) = 0.35$; angle $(end) = 0.59$ als of time t1 = 14; t2 = 14 the first sector: 0.3933465E-02 0
Area of	the second sector: 0.2803914E-01 0



,	"y" then the sour- ; b = 0.450; T = 3		ieu.	
Point bypa Input 0 Input 1-	of Kepler sses 1/4 ellipse c - uniform motion O uniformly accelera elliptical motion	R ted motion OR,	n 89 time units	
Set the e Set the s first se second s interval	tart of the first s and of the first second tor: angle(start) ecto: angle(start) s of time t1= 14; e first sector:	ctor < 3< end < sector <1,, = 0.03; angle <en = 0.89; angle<en t2= 14</en </en 	89):17 89): 55 d)= 0.25	
	second sector:	0.2748918E-01		

Figure 13: Elliptical (Keplerian) movement.

Graphical results of moving a point along an ellipse at different speeds (Figures 14-16).

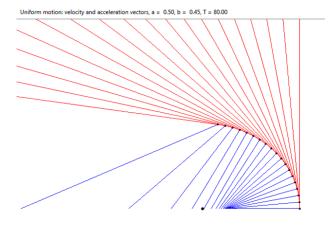
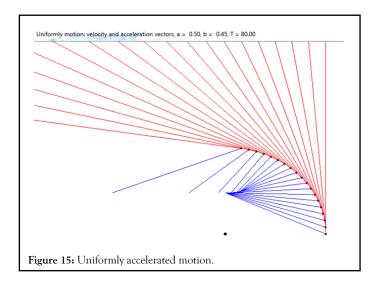
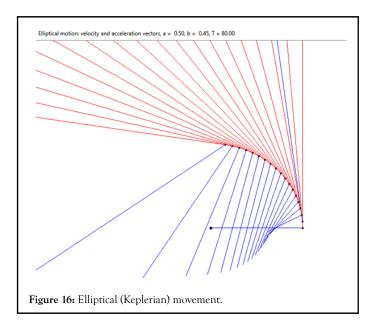


Figure 14: Uniform movement.





Kepler's laws as properties of kinematic equations of motion of a point along curves of the second order

The equations are solved by computer programs. The calculation results are compared with Kepler's laws. The uniqueness of the orbital velocity for the given parameters of the curve is noted. The orbital velocity is calculated from the kinematic equation and compared with the values of astronomical tables.

The sector velocity modulus is a constant for a given ellipse.

$$|v_{\sigma}| = \frac{1}{2}|r| * |v| * \sin(r^{v}) = const$$
(4.1)

If a point moves along a flat curve and its position is determined by the polar coordinates r and $\phi,$ then

$$|v_{\sigma}| = \frac{1}{2} |r|^2 \frac{d\varphi}{dt} = const$$
(4.2)

To illustrate the constancy of the sectoral velocity, a program was written to calculate the sector area in a given time interval. The program, TygeBraheKepler2_focal (A.1), calculates the parameters of the point movement according to equation (8) and shows the equality of the areas of the sectors at equal time intervals (Figures 17–19).

4-angular velocity, 5-polar radius, 6-linear velocity
Enter char =
if char = "y" then the source data is specified: u
ба= 9.00 b = 7.00 dpi = 0.0000000 H = 1.00000005E-03
Second law of Kepler H= 1.00000005E-03
The point bypasses the ellipse in 1/H time units (0 < H < 1), counterclockwise. 1/H = 939
Set the start of the first sector (i0=1,, 999) i0 =
Set the end of the first sector (i0 <i1<1 h)="" i1="<br">999</i1<1>
Set the start of the second sector (0 <i02<1 h-i1+i0)="" i02="</td"></i02<1>
angle(i0) 0.00; angle(i1) 6.28 angle(i02)= 0.00; angle(i12) 6.28
Area of the first sector: 0.1975210E+03
IERR: 0 Area of the second sector: 0.1975210E+03
IERR: 0
Figure 17: Shows the program test The area of the ellipse is π ab

Figure 17: Shows the program test. The area of the ellipse is π ab. 3.14159*9*7=197.92017.

4-angular velocity, 5-polar radius, 6-linear velocity
Enter char =
if char = "y" then the source data is specified:
9 a = 9.00 b = 7.00
dpi = 0.0000000 H = 1.00000005E-03
Second law of Kepler H= 1.00000005E-03
The point bypasses the ellipse in 1/H time units (0 < H < 1), counterclock⊭ise. 1/H ≠ 999
Set the start of the first sector (i0=1,, 999) i0 =
22 Set the end of the first sector (iθ <i1<1 i1="</td" η)=""></i1<1>
333
Set the start of the second sector (0 <i02<1 h−i1+i0)="" i02="<br">555</i02<1>
angle(i0) 0.04; angle(i1) 0.81
angle(i02)= 4.57; angle(i12) 6.03
Area of the first sector: 0.6155315E+02 IERR: 0
Area of the second sector: 0.6155347E+02
IERR: 0

Figure 18: Shows equal time intervals at different points in the period.

On Figure 19 added precession (dpi=0.1) to the parameters of Figure 18. $\,$

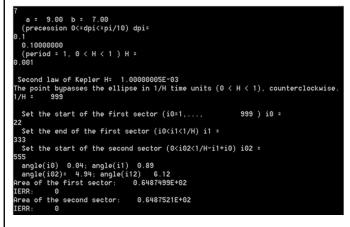


Figure 19: Shows the equality of the areas of the sectors at equal time intervals.

Kepler's third law

At perihelion and aphelion, $sin(\phi)=0$, so the acceleration at these points is zero, and the modulo velocity difference is a constant:

$$v_p - v_a = \delta \tag{4.3}$$

Sector velocity according to the law of conservation of momentum is a constant value:

$$\boldsymbol{v}_{\boldsymbol{s}} = 1/2\,\boldsymbol{v}\mathbf{r} \tag{4.4}$$

Let us express the sector velocity modulo the linear velocity.

Since
$$sin(v_p^{\wedge} r_p) = sin(v_a^{\wedge} r_a)$$
 1, then

$$v_s = 1/2 v_p r_p = 1/2 r_p (v_a + \delta)$$
(4.5)

$$v_s = 1/2 v_a r_a \tag{4.6}$$

$$1/2r_p(v_a + \delta) = 1/2r_a v_a \tag{4.7}$$

$$v_a = \frac{r_p \delta}{r_a - r_p} \tag{4.8}$$

We substitute (4.8) into (4.6):

$$v_s = \frac{\delta r_p r_a}{2(r_a - r_p)} \tag{4.9}$$

Calculate the area of the ellipse. One side:

$$S_{ellipse} = \pi ab$$
 (4.10)

where a is the length of the major semi axis, b is the length of the minor semi axis of the orbit.

On the other hand

$$S_{ellipse} = v_s T = T \frac{\delta r_p r_a}{2(r_a - r_p)}$$
(4.11)

Consequently,

T

$$\frac{\delta r_p r_a}{2(r_a - r_p)} = \pi a b$$

For further transformations, we use the geometric properties of the ellipse. We have ratios: $r_a \cdot r_p = 2c$, c=ae, $r_p r_a = a^2 \cdot c^2 = b^2$.

(4.12)

Substitute into (4.12):

$$\Gamma \frac{\delta b^2}{4ae} = \pi ab \tag{4.13}$$

$$T\frac{\delta b}{a^2 e} = 4\pi$$
; rge $T = 1;$ (4.14)

$$\frac{\delta b}{4\pi a^2 e} = 1 \tag{4.15}$$

Kepler's third law:
$$\frac{T^2}{a^2} = 1$$
 (4.16)

$$\frac{\delta b}{4\pi a^2 e} = \frac{T^2}{a^2} \frac{\delta b}{4\pi e} = \frac{T^2}{a}; T = \frac{1}{2} \sqrt{\frac{\delta b a}{\pi e}} = \frac{1}{2} \sqrt{\frac{(v_p - v_a)ba}{\pi e}}$$
(4.17)

The program Movement of a mat point along an ellipse (A.2), using formulas (4.16) and (4.17), calculates the periods (Figures 20 and 21). $/h_{L}\tilde{a}_{E}$ (au/planet year).

```
The differential equation of the second order curves

with respect to the focus is calculated.

The data table is displayed in the file ellpi.txt.

Table columns:1-number, 2 - time, 3 - engle,

4-engular epeed, 5-polar radius, 6-linear speed

7-engular acceleration, 8-linear acceleration

Enter 0 or 1 or 2 or 3 or 4

0 - enter a, b. Select planet 1 - Mercury, 2 -Uenus, 3 - Earth, 4 - Mars:

0

a :

9

b :

7

a : 9.00 b : 7.00

orbital points (M): 993

period(Kepler3 sqrt(a×x3): 27.000000

period(sqrt(((U1-U2)×b×a)/(pi×x1)/2) : 26.999981

pAUSE

To resume execution, type go. Other input will terminate the job.

Figure 20: The differential equation of the second order curves.
```

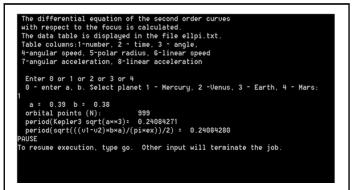
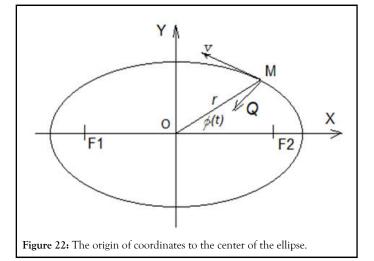


Figure 21: The differential equation of the second order curves with respect to the focus is calculated.

Differential equation of motion of a point along an ellipse with respect to the center

Let's move the origin of coordinates to the center of the ellipse, Figure 22. The radius function (2.7) will change.



M-Material point. Q is a generalized force acting on a point. O-center, v-linear speed of the point. $\phi(t)$ is the angle between the X-axis and the point, counterclockwise.

Kepler's second law

The TygeBraheKepler2_center (A.1) program calculates the parameters of the point movement according to equations (2.7–2.13), and shows the equality of the areas of the sectors at equal time intervals (Figures 23–25).

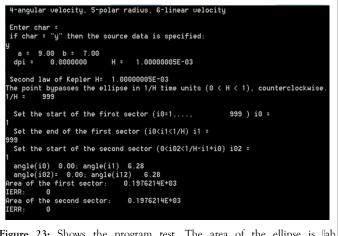


Figure 23: Shows the program test. The area of the ellipse is lab. 2*3.14159*9*7=197.92017

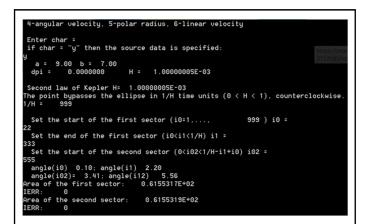


Figure 24: Equal time intervals are given at different moments of the period.

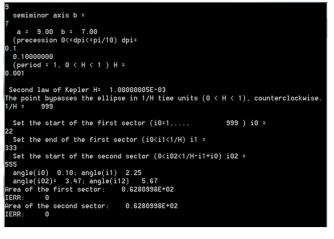


Figure 25: Added precession to the parameters.

On figure 25 added precession (dpi=0.1) to the parameters of figure 23.

Kepler's third law

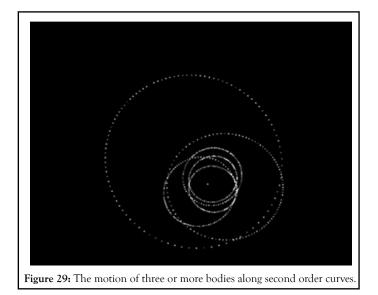
The program movement of a mat point along an ellipse center (A.2), using formulas (4.16-4.17), calculates the periods. δ =v1-v2 (au/planet year).

In Figures 25-30 we see that with an increase in the eccentricity, the difference between the periods increases.

The differential equation of the second order curves with respect to the focus is calculated. The data table is displayed in the file ellpi.txt. Table columns:1-number, 2 - time, 3 - angle, 4-angular speed, 5-polar radius, 6-linear speed 7-angular acceleration, 8-linear acceleration
Enter 0 or 1 or 2 or 3 or 4 o - enter a, b. Select planet 1 - Mercury, 2 -Venus, 3 - Earth, 4 - Mars: a = 9
<pre>b = 7 a = 9.00 b = 7.00 orbital points (N): 999 period(Kepler3 sqrt(a×x3)= 27.000000 period(sqrt(((U-u2)kbxa)/(pi×ex))/2) = 21.000002</pre>
Polos Polos To resume execution, type go. Other input will terminate the job.
Figure 26: The program movement of a mat point along an ellipse center.



Figure 28: Shows the equality of the areas of the sectors at equal time intervals.



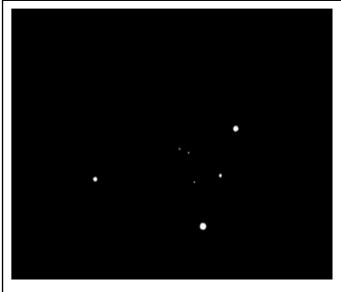


Figure 30: For modeling streamlines of liquid and gas particles.

CONCLUSION

The kinematic equation (1.10) accurately describes the motion along ideal second order curves. The real orbits of cosmic bodies have deviations from the ideal curve: Precession, periodic asymmetry of the lengths of the radii, and other types of deviation.

Equation (1.10) and the center of mass theorem make it possible to simulate the motion of three or more bodies along second order curves.

The kinematic equation (2.13) is applicable for modeling streamlines of liquid and gas particles.

The article used materials from textbooks on mechanics.

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